

the resulting crack is shown in figure 7a. as the crack is relatively small compared to the  $c_j$  width, it is captured with a single planar view. the crack has the typical v-shape of a notch. a stress contour map and the corresponding von mises stress distribution are shown in figure 7b. the notch acts as a compressive prestress element in the  $c_j$ , which induces a compressive stress field in the neck region of the  $c_j$ . since the neck is formed by the electrode-bridge, the shape of the crack is determined by the edge geometry of the electrode-bridge. as the neck of the electrode-bridge is tapered, a high compressive stress is induced in the neck, as indicated in figure 7b. since the peak compressive stress occurs at the middle of the electrode-bridge, a crack is formed at the middle of the electrode-bridge. overall, the stress distribution in the neck is asymmetric in the cross-sectional plane, and the crack is not transverse. the asymmetry of the peak compressive stress is associated with the geometry of the  $c_j$ , as shown in figure 4. the asymmetry of the peak compressive stress is associated with the geometry of the  $c_j$ , as shown in figure 5, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=1.7\text{m}$  and  $w=280\text{nm}$ . as shown in figure 5, the stress distribution in the neck becomes asymmetric with a peak compressive stress which is larger on the left side of the notch. this asymmetry is further amplified in figure 5, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=1$ . this asymmetry is further amplified in figure 6, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=1$ . as shown in figure 6, the stress distribution in the neck becomes asymmetric with a peak compressive stress which is larger on the left side of the notch. this asymmetry is further amplified in figure 7, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=1$ . as shown in figure 7, the stress distribution in the neck becomes asymmetric with a peak compressive stress which is larger on the left side of the notch. this asymmetry is further amplified in figure 8, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=1$ . as shown in figure 8, the stress distribution in the neck becomes asymmetric with a peak compressive stress which is larger on the left side of the notch. the crack is transverse, and the stress distribution in the neck becomes symmetric as the crack grows, as shown in figure 9, where the stress map and the corresponding von mises stress distribution are shown for a  $c_j$  with  $l=2.1\text{m}$  and  $w=280\text{nm}$ .

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## 2020 Design V10 Crack

experimental results to evaluate the effect of the notch design on crack formation, 3d-printed cjs were fabricated, corresponding to the five columns of the matrix. in the first column, the cjs were designed with the notch indent  $t=0\text{nm}$ , while in the second column the  $t$  was increased to  $40\text{nm}$ . in the third column, the  $t$  was increased to  $100\text{nm}$  and, in the fourth column, the  $t$  was increased to  $180\text{nm}$ . to evaluate the reproducibility of the results, all cjs were fabricated four times, each time with a different design. the fabricated cjs are shown in figure 8a. the crack formation is color-coded, with the red coloring indicating cracks that have not yet emerged and the green coloring indicating cracks that have already emerged. in the cjs designed with the notch indent  $t=0\text{nm}$ , the cracks do not yet emerge, as indicated by the red coloring of the electrodes. in the cjs designed with the notch indents of  $t=40\text{nm}$ ,  $100\text{nm}$  and  $180\text{nm}$ , the cracks emerge at the constriction area of the electrode-bridge for all four specimens of each cj. these results are consistent with the k tn analysis of the critical notch indent  $t$  that defines a fracture threshold. in the cjs designed with the notch indent  $t=0\text{nm}$ , the critical  $t$  is clearly smaller than  $40\text{nm}$ , suggesting that the fracture threshold is around  $t=40\text{nm}$ . in the cjs designed with the notch indent  $t=40\text{nm}$ , the critical  $t$  is about  $40\text{nm}$ , as is expected from the k tn analysis. in the cjs designed with the notch indent  $t=100\text{nm}$ , the critical  $t$  is about  $100\text{nm}$ , while in the cjs designed with the notch indent  $t=180\text{nm}$ , the critical  $t$  is about  $180\text{nm}$ . Sec8ef588b

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